

ZsimOpt training

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Identification of material coefficients



- Identification of the constitutive equations (Chaboche model)
- Identification of viscoplastic behavior of IN738 for each temperature (20°C, 300°C, 500°C, 700°C, 850°C)
 - Calibration of the viscous effect on monotonic tests
 - Calibration of isotropic and kinematic hardenings on cyclic tests
- Fit analytical functions on the coefficients temperature evolution
- Identification of analytical functions coefficients on the whole database
- Verification on anisothermal tests

Plan

1 Experimental database

2 Material model

3 Calibration strategy



Plan

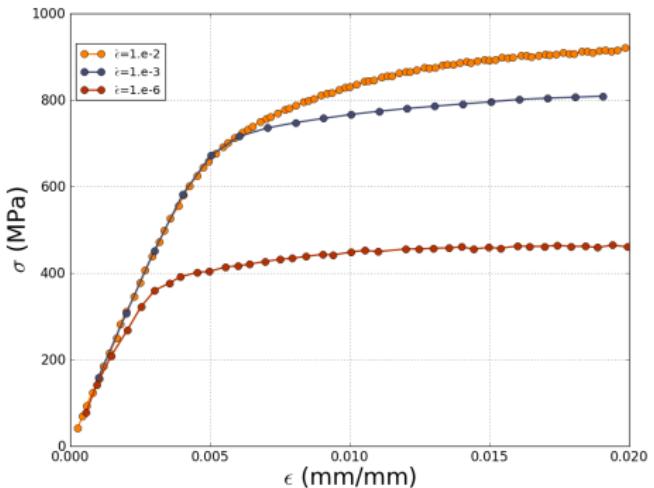
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Experimental database

Tensile tests at various strain rates



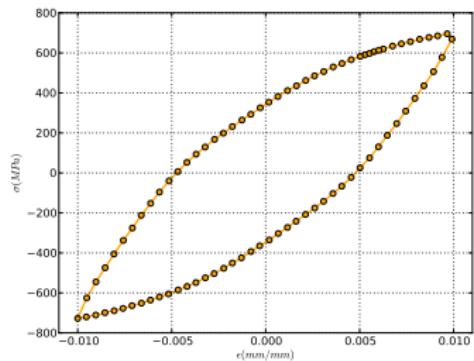
- EXP/tenx2.exp – strain rate $1.e-2\text{ s}^{-1}$
- EXP/tenx3.exp – strain rate $1.e-3\text{ s}^{-1}$
- EXP/tenx6.exp – strain rate $1.e-6\text{ s}^{-1}$

Experimental data base

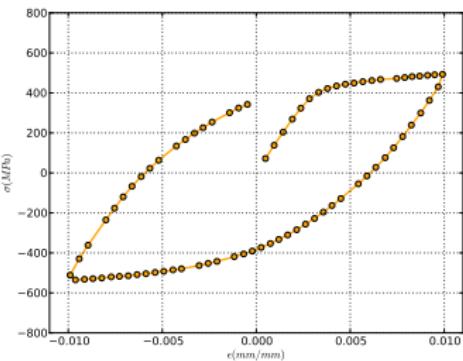


Strain controlled cyclic tests, $\epsilon = [-0.01 : 0.01]$

$$\dot{\epsilon} = 10^{-3} \text{ s}^{-1}$$



$$\dot{\epsilon} = 10^{-5} \text{ s}^{-1}$$

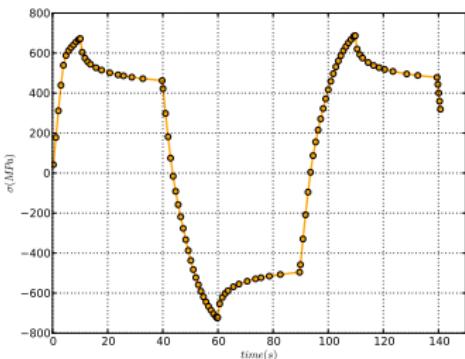
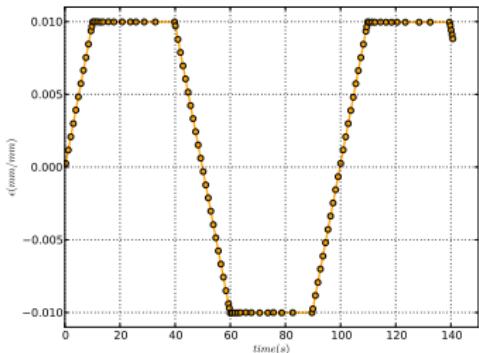


- EXP/lcf1x3.exp – strain rate $1.e-3 \text{ s}^{-1}$
- EXP/lcf1x5b.exp – strain rate $1.e-5 \text{ s}^{-1}$

Experimental data base



- Strain controlled cyclic+relaxation tests, $\epsilon = [-0.01 : 0.01]$

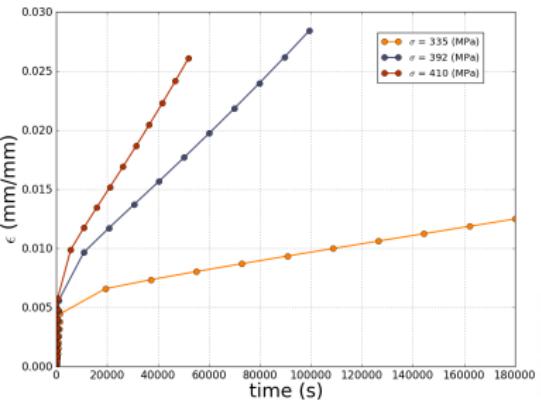
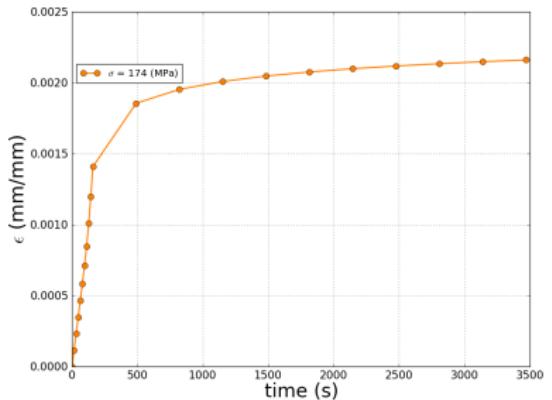


- EXP/frix3.exp – strain rate 0.001/s

Experimental data base



Creep tests



- EXP/cr174.exp : $\sigma=174 \text{ MPa}$
- EXP/cr335.exp : $\sigma=335 \text{ MPa}$
- EXP/cr392.exp : $\sigma=392 \text{ MPa}$
- EXP/cr410.exp : $\sigma=410 \text{ MPa}$

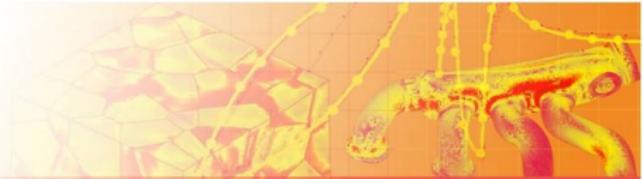
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The Chaboche model



- $\tilde{\epsilon}^e$ and $\tilde{\epsilon}^{vp}$ are the elastic and viscoplastic strain tensors,
- $\tilde{\epsilon}^{th}$ is the thermal strain,
- $J(\cdot)$ is the von Mises invariant of a second-order tensor,
- v is the plastic multiplier (cumulated viscoplastic deformation),
- n is the normal to the yield surface.

Strain partition:

$$\tilde{\epsilon} = \tilde{\epsilon}^e + \tilde{\epsilon}^{th} + \tilde{\epsilon}^{vp}$$

Elasticity:

$$\tilde{\sigma} = \tilde{E} : \tilde{\epsilon}^e$$

Plasticity criterion:

$$f(\tilde{\sigma}) = J(\tilde{\sigma}_{eff}) - R \quad \text{with} \quad \tilde{\sigma}_{eff} = \tilde{\sigma} - \tilde{X}$$

Norton flow rule:

$$\dot{v} = \left\langle \frac{f(\tilde{\sigma})}{K} \right\rangle_n$$

Normality rule:

$$\dot{\epsilon}^{vp} = \dot{v} n \quad \text{with} \quad n = \frac{3}{2} \frac{dev(\tilde{\sigma}_{eff})}{J(\tilde{\sigma}_{eff})}$$

Non-linear kinematic hardening:

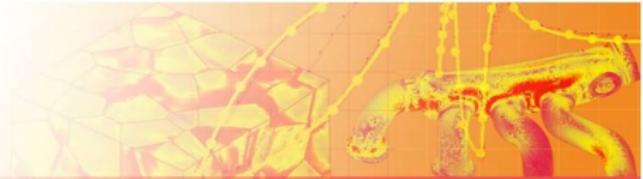
$$\tilde{X} = \frac{2}{3} C \alpha \quad , \quad \dot{\alpha} = \dot{v} (n - D \alpha)$$

Constant isotropic hardening:

$$R = R_0$$

5 coefficients for each temperature : K, n, R_0, C, D

The Chaboche model



- Additional visco-plastic potential for creep behavior (slow evolutions)

Strain partition:

$$\dot{\epsilon} = \dot{\epsilon}^e + \dot{\epsilon}^{th} + \dot{\epsilon}^{vp} + \dot{\epsilon}_s^{vp}$$

Norton flow rule:

$$\dot{v}_s = \left\langle \frac{f(\sigma)}{K_2} \right\rangle$$

Normality rule:

$$\dot{\epsilon}_s^{vp} = v_s \mathbf{n} \quad \text{with} \quad \mathbf{n} = \frac{3}{2} \frac{\text{dev}(\tilde{\sigma}_{\text{eff}})}{J(\tilde{\sigma}_{\text{eff}})}$$

Constant isotropic hardening: $R = R_{02} = 0$

2 more coefficients for each temperature : K_2, n_2

Plan

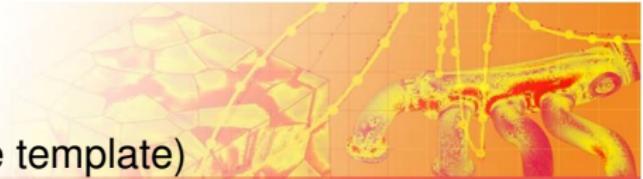
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Calibration strategy



- load Chaboche model (create template)
- load experiments
- optimization on tensile tests, first potential
 - create simulations
 - create optimizations
 - no kinematic hardening ($C=1.$), optimize K, n, R_0
- optimization on cyclic tests (including cyclic+relaxation tests), first potential
 - create simulations
 - create optimizations
 - n - fixed, optimize K, R_0, C, D
 - release n and optimize n, K, R_0, C, D
- optimization on creep tests, second potential
 - create simulations
 - create optimizations
 - n, K, R_0, C, D - fixed, optimize n_2, K_2